

**Final Report**  
**Calibration-Round-Robin**  
**CaRo 00/01**

**Adolf Kühner AG**  
**Dinkelbergstr. 1**  
**CH-4127 Birsfelden**  
**Switzerland**

**Tel. +41 (0)61 319 93 93**  
**Fax. +41 (0)61 319 93 94**  
**E-mail office @ kuhner.com**  
**Internet www.kuhner.com**

This report shall not be published or reproduced other than in full.

## Conclusion

---

According to international standards (e.g. ISO 9000, GLP), test equipment must be calibrated at intervals by comparison with a standard or a calibrated testing apparatus.

This calibration also applies to the 20-l-apparatus and the 1-m<sup>3</sup>-vessel for the determination of P<sub>max</sub> and K<sub>max</sub> and the apparatus for determination of the minimum ignition energy. The test procedure is an important part of this calibration. A general check at the component level is incomplete and hence inadmissible.

Unfortunately there are neither internationally recognized reference samples nor reference equipment available for the determination of these explosion characteristics. Therefore the following calibration method has been carried out successfully:

A dust has been selected, prepared and supplied to **42** test laboratories all over the world. The mean values of the explosion indices, measured by the participating laboratories, has been calculated as reference values. The testing laboratories have been informed about the evaluation with a certificate.

This report presents the results of this calibration method and describes the evaluation procedures. It also demonstrates that with this method it was possible to discover and rectify the cause of any errors with installations producing results differing widely from the reference values.

### CaRo 00/01 - Reference values for the Explosion Indices P<sub>max</sub> and K<sub>max</sub>

<b>P<sub>max</sub></b> (bar)	<b>8.4 ± 10%</b> (7.5 ... 9.2)
<b>K<sub>max</sub></b> (bar·m/s)	<b>220 ± 10%</b> (198 ... 242)

### CaRo 00/01 - Reference values for the Minimum Ignition Energy MIE

<b>Es / 3</b>	<b>Es</b>	<b>Es • 3</b>
<b>4 mJ</b>	<b>12 mJ</b>	<b>36 mJ</b>



Birsfelden, November 2001

Adolf Kühner AG  
Christoph Cesana

## Participants

---

For details see section "list of participants".

	Pmax, Kmax (42)					MIE (27)	
	8.4-1	20-1	1 m <sup>3</sup>	1.2 m <sup>3</sup>	2.4 m <sup>3</sup>	MIKE	others
Austria		1				1	
Australia	1						
Belgium		2				1	
Germany		9	2	1		6	2
England		3					1
Finland		1					
France		5				3	
Holland		1					
Hungary							1
Italy						1	
Japan						1	
Canada		1				1	
Norway		3					1
Switzerland		5	1		1	6	
Spain		1					
South Africa		1					
U.S.A.		2	1			2	
<b>total:</b>	<b>1</b>	<b>35</b>	<b>4</b>	<b>1</b>	<b>1</b>	<b>22</b>	<b>5</b>

This calibration round robin test „CaRo 00/01“ has been accepted world wide as the best and most reliable calibration method for this type of test equipment.

## Test substance

---

For correct calibration the CaRo 00/01 test sample has been milled, homogenized and shipped in an air tight package. Therefore the sample has to be tested „as delivered“.

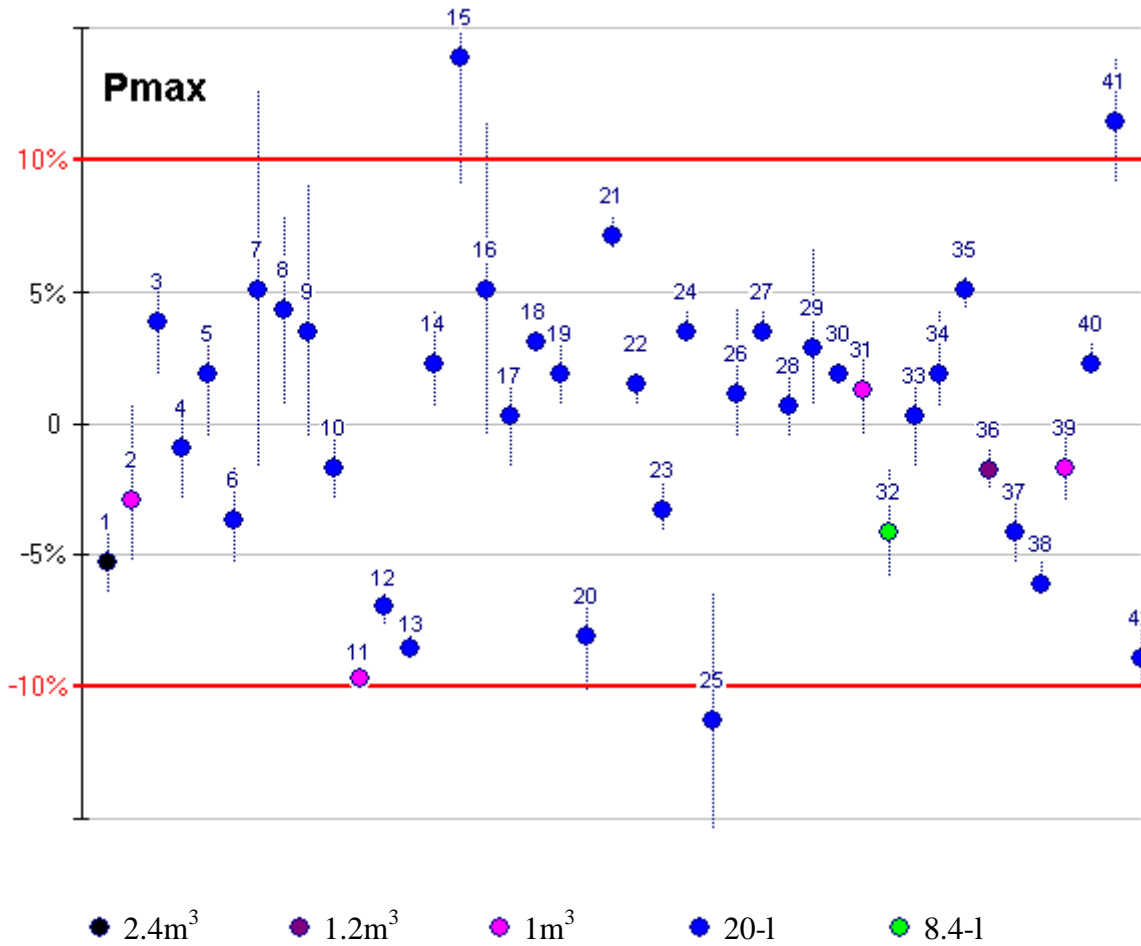
**CaRo 00/01 = Niacinamide USP DC (Pyridine-3-carboxamide)**

### Particle size distribution:

d (0.1)	d (0.5)	d (0.9)
10% of particles	50% of particles	90% of particles
<b>&lt; 14 µm</b>	<b>&lt; 40 µm</b>	<b>&lt; 90 µm</b>

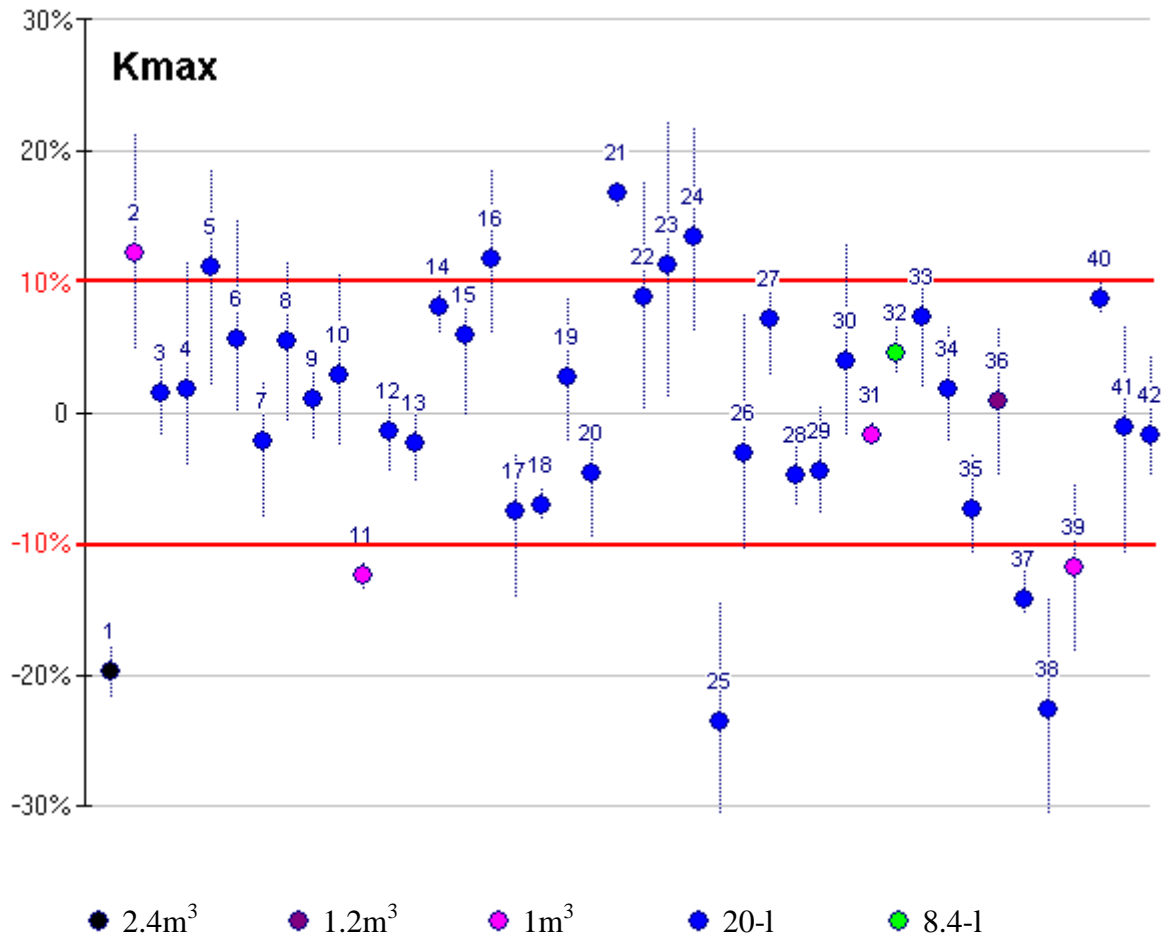
## Explosion Indices Pmax, Kmax

**Pmax = 8.4 bar ± 10%** (7.5 ... 9.2)



The individual results are drawn in relation to the arithmetic mean of all results and in chronological sequence (number of certificate).

**Kmax = 220 bar·m/s ± 10% (198 ... 242)**



The individual results are drawn in relation to the arithmetic mean of all results and in chronological sequence (number of certificate).

**Test procedure:**

The method for determination of  $P_{max}$ ,  $K_{max}$  is described in the „Manual CaRo 00“.

**Evaluation:**

The explosion indices  $P_{max}$  and  $(dP/dt)_{max}$  are defined as the mean values of the maximum values of each series. Subsequently, the explosion index  $K_{max}$  is calculated from the mean value  $(dP/dt)_{max}$ .

**Scatter of  $P_{max}$  and  $K_{max}$** 

The maxima of each series must not deviate by more than **10%** of  $P_{max}$  resp.  $K_{max}$ . Otherwise this series must be repeated !

**Calculation of the reference values:**

First the mean values of all test results (41) has been calculated. In a 2nd step all results outside of the tolerance band are excluded prior to the subsequent calculation of the mean value. Due to the large number of participants the mean values did not change.

**Cause of errors:**

Some laboratories has to repeat the tests. The reasons are:

- a) Faulty gauge (vacuum, pressure of dust storage chamber)
- b) Leaky apparatus (o-ring, ball valve)
- c) Ignition delay time (large vessel)

**Dust distribution:**

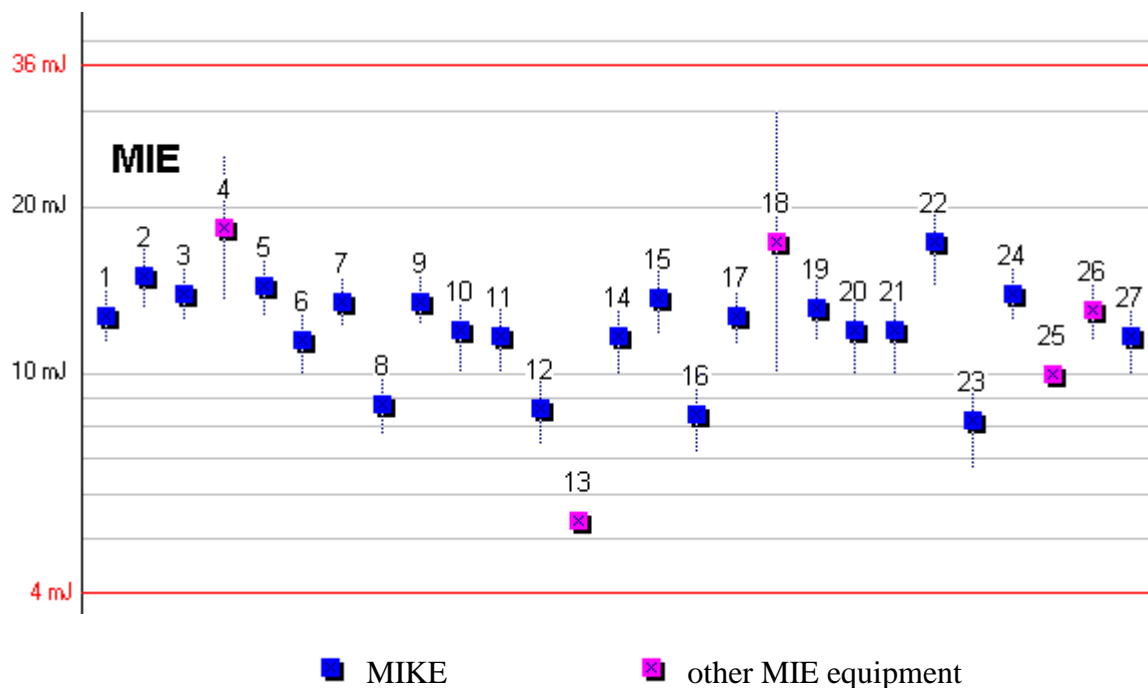
20-l-apparatus with rebound nozzle: 33  
 20-l-apparatus with ring nozzle: 2  
 Large vessels with ring nozzle: 6 (all)

**Large vessels:**

Remarkable are the different ignition delay times ( $t_v$ ) dependent from the type of valve and volume of the vessel:

	tv (ms)	volume	apparatus
Valve with blasting cap activation:	600	1m <sup>3</sup>	2
Valve with electro pneumatic drive:	550	1m <sup>3</sup>	2
Valve with electro pneumatic drive:	700	1.2m <sup>3</sup>	1

## Minimum Ignition Energy MIE



The individual results are drawn in chronological sequence (number of certificate).

### Test procedure:

The method for determination of the MIE is described in the „Manual CaRo 00/01“.

### Estimation of the statistical energy (Es):

The minimum ignition energy MIE lies, by definition, between two energy values:

$$E1 < MIE < E2$$

For the purpose of comparison between different apparatus, only one MIE value (Es) instead of the energy range (E1, E2) shall be used. This single value (Es) can be estimated by use of the probability of ignition as follows (prEN 13821):

Provided that for the energy E2 a minimum of 5 dust concentrations evenly distributed are tested, the position of the MIE in the E1-E2 range can be estimated. At ignition energy E2, the number of dust concentrations with ignition, is divided by the total number of dust concentrations tested.

$$Es = 10^{(\log E2 - I[E2] \cdot (\log E2 - \log E1) / ((NI+I)[E2] + 1))}$$

where is:  
 $I[E2]$  = number of tests with ignition at the energy E2.  
 $(NI+I)[E2]$  = total number of tests at the energy E2.

Dependent from the data received, the following methods has been applied:

no	data	method of Es-estimation:
23	E1, E2, I, NI	$Es = 10^{(\log E2 - I[E2] \cdot (\log E2 - \log E1) / ((NI+I)[E2]+1))}$
4	E1, E2	$Es = 10^{((\log E2 + \log E1) / 2)}$

### Criteria for conformity:

Conformity between two equipment (a, b) is given, when the Es-values differ less than a factor of 3 (prEN 13821).

$$1/3 < Es(a) / Es(b) < 3$$

Accordingly:

Conformity in the CaRo 00/01 is given, when the Es-value of each equipment differ less than a factor of 3 to the mean (Es) of all equipment:

<b>Es / 3</b>	<b>Es</b>	<b>Es • 3</b>
<b>4 mJ</b>	<b>12 mJ</b>	<b>36 mJ</b>

The criteria for conformity has been fulfilled by all laboratories.



## List of Participants

---

Country	Company Laboratory	E-Mail	Pmax Kmax	MIE
Austria	AUVA Allg. Unfallversicherungsanstalt	klaus.kopia@auva.sozvers.at	✓	✓
Australia	WorkCover NSW TestSafe Australia	david.pearson@workcover.nsw.gov.au	✓	
Belgium	D.D. Engineering	ddeng@online.be	✓	
Belgium	Katholieke Universiteit Leuven	jan.berghmans@mech.kuleuven.ac.be	✓	✓
Germany	BASF Aktiengesellschaft	markus.goedde@basf-ag.de	✓	✓
Germany	BGN Zentrallabor	m.roser.bgn.versuchsanlage@t-online.de	✓	✓
Germany	B I A Staubexplosionslabor	h.beck@hvbv.de	✓	✓
Germany	Boehringer Ingelheim Pharma KG AVE-Sicherheits- und Materialprüf- stelle	thomas.habermann@ing.boehringer- ingelheim.com	✓	✓
Germany	FH Merseburg / Uni Halle SiTech	frank.ramhold@cui.fh-merseburg.de	✓	
Germany	Henkel KGaA VTA-Sicherheitstechnik	michael.schrieber@denotes.henkel.de	✓	✓
Germany	IBExU GmbH Staublabor	post@ibexu.de	✓	✓
Germany	Schering AG Chem. Sicherheitsprüfungen	fernando.lopezholguin@schering.de	✓	
Germany	Wacker Chemie GmbH Stabex, Zentrale Analytik	markus.haider@wacker.com		✓
Germany	Wilhelm-Jost-Institut e.V. Explo- sions- und Brandschutz	wji@wji.de	✓	✓
England	Anonym		✓	
England	Building Research Establishment	manchesters@bre.co.uk	✓	✓
England	GlaxoSmithKline Hazard Determination Laboratory	michael.i.gilmore@gsk.com	✓	
Finland	VTT Building and Transport, Fire Technology	johan.mangs@vtt.fi	✓	
France	Aventis Pharma Département Sécurité des Procédés	andre.guilland@aventis.com	✓	✓
France	Anonym		✓	
France	ENSIC, LSGC	perrin@ensic.inpl-nancy.fr	✓	
France	INERIS	mohamed.boudalaa@ineris.fr	✓	
France	Rhoditech Process Safety Laboratory	joseph-marc.francois@eu.rhodia.com	✓	✓
France	SNPE, DFP/TCFC	i.laine@SNPE.com		✓
Holland	DSM, DSM Research	eddy.oost-van-t@dsm-group.com	✓	
Hungary	Gedeon Richter Ltd Safety Laboratory	gy.negyesei@richter.hu		✓

Country	Company Laboratory	E-Mail	Pmax Kmax	MIE
Italy	Stazione sperimentale Combustibili Sicurezza	mazzei@ssc.it		✓
Japan	TIIS, The Technology Institution of Industrial Safety Asaka Safety Test Laboratory	kasuya@ankyoo.or.jp		✓
Canada	Dalhousie University Department of Chemical Engineering	paul.amyotte@dal.ca	✓	✓
Norway	GexCon AS	oysteintl@gexcon.com	✓	✓
Norway	University of Bergen, Dust Laboratory	trygve.skjold@fi.uib.no	✓	
Switzerland	CIMO SA Laboratoire de sécurité	serge.pythoud@cimo-sa.ch	✓	✓
Switzerland	Firmenich SA Safety Laboratory - DCDC	franco.ferregutti@firmenich.com	✓	
Switzerland	Lonza AG Sicherheitslabor	eberhard.irle@lonzagroup.com	✓	
Switzerland	Sicherheitsinstitut, Basel Prüflabor	abisel@swissi.ch	✓	✓
Spain	Laboratorio Oficial J.M. Madariaga (LOM)	jgtorrent@qyc.upm.es	✓	
South Africa	CSIR South Africa Explosion Laboratory	ikessler@csir.co.za	✓	
U.S.A.	Eli Lilly & Co Chemical Hazards Laboratory	creeden_daniel_j@lilly.com	✓	✓
U.S.A.	Fike Corporation	sjohnson@fike.com	✓	
U.S.A.	Merck & Co., Inc. Process Safety Lab.	michael_toth@merck.com	✓	✓